# Drift- 

# PREPARED ESPECIALLY FOR UNAVCO 

B-901

September 12, 2007


This Wellbore DRIFT Interpretation Package represents our best efforts to provide a correct interpretation. Nevertheless, since all interpretations are opinions based on inferences from electrical or other types of measurements, we cannot and do not guarantee the accuracy or correctness of any interpretation, and we shall not be liable or responsible for any loss, costs, damages, or expenses incurred or sustained by Customer resulting from any interpretation made by this document. Welenco does not warrant or guarantee the accuracy of the data, specifically including (but without limitations) the accuracy of data transmitted by electronic process, and Welenco will not be responsible for accidental or intentional interception of such data by third parties. Welenco employees are not empowered to change or otherwise modify the attached interpretation. By accepting this DRIFT Interpretation Package, the Customer agrees to the foregoing, and to the General Terms and Conditions of Welenco.

| Company: UNAVCO |  | County: Monterey | State: California |
| :---: | :---: | :---: | :---: |
| Well Number: B-901 | Well Owner: | Survey Date: September 12, 2007 | Magnetic Declination: Not Used |
| Field: Indian Springs |  | Operator:_Mitch tullis | Casing Size: 6" |
| Van No.: L-18 | Job Ticket: | Welenco Office: Santa Ynez | Witness: Sarah Venator |
| Location: |  |  |  |
| Remarks: |  | Tool Type: Gyroscopic | Tool No.: |

Methodology:
Balanced Tangential
Lat.: $35^{\circ} 41^{\prime} 22.8^{\prime \prime}$
Long.: $120^{\circ} 8^{\prime} 28.2^{\prime \prime}$ Sec: 9
Twp: 26S Rge: 17E Meridian: Mt. Diablo
(NOTE: Latitude and Longitude values were determined using a recreational GPS accurate to $+/-45$ feet. The Section, Township, Range and Meridian then determined using the TRS conversion program (TRS accuracy is not guaranteed).)

| Measured Data |  |  | Drift Computations |  |  |  | Rectangular Computations |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth, Feet | Inclination, Degrees From Vertical | Azimuth, Degrees, True | Course Deviation, Feet | True Vertical Depth, Feet | Drift Distance, Feet | Drift <br> Bearing, <br> Degrees, True | Latitude, Feet | Departure, Feet | Total Latitude, Feet | Total Departure, Feet |
| 390' | $2.08{ }^{\circ}$ | $313^{\circ}$ | 0.00' | 390.00' | 0.00' (.00') | 00.00 ${ }^{\circ}$ | .00' | 0.00' | .00' | 0.00' |
| 395' | $2.14{ }^{\circ}$ | $182^{\circ}$ | 0.08' | 394.99' | 0.08' (.96") | $245.70^{\circ}$ | -.03' | -0.07' | -.03' | -0.07' |
| 400' | $1.55^{\circ}$ | $245^{\circ}$ | $0.14{ }^{\prime}$ | 399.98' | 0.20' (2.40') | $221.40^{\circ}$ | -.12' | -0.07' | -.15' | -0.14' |
| 405' | $1.98{ }^{\circ}$ | $196{ }^{\circ}$ | $0.14{ }^{\prime}$ | 404.97' | 0.34' (4.08") | $219.80^{\circ}$ | -.11' | -0.09' | -.27' | -0.22' |
| 410' | $2.25{ }^{\circ}$ | $198{ }^{\circ}$ | 0.18' | 409.96' | 0.52' (6.24') | $211.80^{\circ}$ | -.18' | -0.05' | -.44' | -0.27' |
| 415' | $2.58{ }^{\circ}$ | $196{ }^{\circ}$ | 0.21' | 414.95' | 0.72' (8.64") | $207.60{ }^{\circ}$ | -.20' | -0.06' | -.64' | -0.34' |
| 420' | $2.64{ }^{\circ}$ | $192^{\circ}$ | 0.23' | 419.94' | 0.95 (11.40') | $204.30^{\circ}$ | -.22' | -0.06' | -.86' | -0.39' |
| 425' | $2.43{ }^{\circ}$ | $190^{\circ}$ | 0.22' | 424.93' | 1.16' (13.92') | $201.80^{\circ}$ | -.22' | -0.04' | -1.08' | -0.43' |
| 430' | $2.45{ }^{\circ}$ | $192^{\circ}$ | 0.21' | 429.92' | 1.37 ' (16.44") | $200.10^{\circ}$ | -.21' | -0.04' | -1.29' | -0.47' |
| 435' | $2.41^{\circ}$ | $190^{\circ}$ | 0.21' | 434.91' | 1.58 ' (18.96") | $198.90^{\circ}$ | -.21' | -0.04' | -1.50' | -0.51' |
| 440' | $2.48{ }^{\circ}$ | $191^{\circ}$ | 0.21' | 439.90' | 1.79' (21.48") | $197.90^{\circ}$ | -.21' | -0.04' | -1.71' | -0.55' |
| 445' | $2.70^{\circ}$ | $186^{\circ}$ | 0.23' | 444.89' | 2.02' (24.24") | $196.90^{\circ}$ | -.22' | -0.03' | -1.93' | -0.59' |
| 450' | $2.83{ }^{\circ}$ | $182^{\circ}$ | 0.24' | 449.88' | 2.25' (27.00") | $195.50^{\circ}$ | -.24' | -0.02' | -2.17' | -0.60' |
| 455' | $2.96{ }^{\circ}$ | $182^{\circ}$ | 0.25' | 454.87' | $2.50{ }^{\prime}\left(30.00{ }^{\prime \prime}\right)$ | $194.10^{\circ}$ | -.25' | -0.01' | -2.42' | -0.61' |
| 460' | $2.86{ }^{\circ}$ | $180^{\circ}$ | 0.25' | 459.86' | $2.75{ }^{\prime}$ (33.00') | $193.00^{\circ}$ | -.25' | -0.01' | -2.68' | -0.62' |
| 465' | $2.67^{\circ}$ | $181^{\circ}$ | 0.24' | 464.85' | $2.98{ }^{\prime}$ (35.76") | $192.00^{\circ}$ | -.24' | 0.00' | -2.92' | -0.62' |
| $470{ }^{\prime}$ | $2.90^{\circ}$ | $185^{\circ}$ | 0.24' | 469.84' | 3.22' (38.64") | $191.30^{\circ}$ | -.24' | -0.01' | -3.16' | -0.63' |
| 475' | $2.68{ }^{\circ}$ | $182^{\circ}$ | 0.24' | 474.83' | 3.46 ' (41.52") | $190.80^{\circ}$ | -.24' | -0.02' | -3.40' | -0.65' |
| 480' | $2.68{ }^{\circ}$ | $182^{\circ}$ | 0.23 ' | 479.82' | 3.70' (44.40') | $190.20^{\circ}$ | -.23' | -0.01' | -3.64' | -0.65' |
| 485' | $2.77^{\circ}$ | $183^{\circ}$ | 0.24' | 484.81' | 3.93' (47.16") | $189.70^{\circ}$ | -.24' | -0.01' | -3.87 | -0.66' |
| 490' | $3.31{ }^{\circ}$ | $183^{\circ}$ | 0.27' | 489.80' | 4.19' (50.28") | $189.30^{\circ}$ | -.27' | -0.01' | -4.14' | -0.68' |
| 495' | $2.92{ }^{\circ}$ | $183^{\circ}$ | 0.27' | 494.79' | 4.46' (53.52') | $188.90^{\circ}$ | -.27' | -0.01' | -4.41' | -0.69' |
| 500' | $3.91{ }^{\circ}$ | $181^{\circ}$ | 0.30' | 499.78' | 4.76 ' (57.12") | $188.50^{\circ}$ | -.30' | -0.01' | -4.71' | -0.70' |
| 505' | $2.61{ }^{\circ}$ | $177^{\circ}$ | 0.28' | 504.77' | 5.04' (60.48") | $188.00^{\circ}$ | -.28' | 0.00' | -4.99' | -0.70' |
| 510' | $3.00^{\circ}$ | $182^{\circ}$ | 0.24' | 509.76' | 5.28' (63.36") | $187.60^{\circ}$ | -.24' | 0.00' | -5.24' | -0.70' |
| 515' | $3.01{ }^{\circ}$ | $179^{\circ}$ | 0.26' | 514.75' | 5.54' (66.48") | $187.30^{\circ}$ | -. 26 ' | 0.00' | -5.50' | -0.70' |
| 520' | $2.50^{\circ}$ | $175^{\circ}$ | 0.24' | 519.74' | 5.78' (69.36") | $186.80^{\circ}$ | -.24' | 0.01' | -5.74' | -0.69' |

New Solutions in Borehole Geophysics

## Wellbore Drift Interpretation

## welenco <br> (800) 445-9914


(NOTE: Latitude and Longitude values were determined using a recreational GPS accurate to + +- 45 feet. The Section, Township, Range and Meridian then determined using the TRS conversion program (TRS accuracy is not guaranteed).)

| Measured Data |  |  | Drift Computations |  |  |  | Rectangular Computations |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth, Feet | Inclination, Degrees From Vertical | Azimuth, Degrees, True | Course Deviation, Feet | True Vertical Depth, Feet | Drift Distance, Feet | Drift <br> Bearing, Degrees, True | Latitude, Feet | Departure, Feet | Total Latitude, Feet | Total Departure, Feet |
| 525' | $3.02{ }^{\circ}$ | $181^{\circ}$ | 0.24' | 524.73' | 6.02' (72.24") | $186.50^{\circ}$ | -.24' | 0.01' | -5.98' | -0.68' |
| 530' | $2.43{ }^{\circ}$ | $191^{\circ}$ | 0.24' | 529.72' | 6.25 ( $75.00{ }^{\prime \prime}$ ) | $186.50^{\circ}$ | -.24' | -0.02' | -6.21' | -0.70' |
| 535' | $3.02{ }^{\circ}$ | $175^{\circ}$ | 0.24' | 534.71' | 6.49 ' (77.88") | $186.30^{\circ}$ | -.24' | -0.01' | -6.45' | -0.71' |
| 540' | $2.67^{\circ}$ | $185^{\circ}$ | 0.25' | $539.70{ }^{\prime}$ | $6.73{ }^{\prime}$ (80.76") | $186.10^{\circ}$ | -.25' | 0.00' | -6.70' | -0.71' |
| 545' | $2.06{ }^{\circ}$ | $179^{\circ}$ | 0.21' | 544.69' | 6.94' (83.28') | $186.00^{\circ}$ | -.21' | -0.01' | -6.90' | -0.72' |
| 550' | $3.16{ }^{\circ}$ | $195^{\circ}$ | 0.23' | 549.68' | 7.16' (85.92') | $186.10^{\circ}$ | -.22' | -0.03' | -7.13' | -0.76' |
| 555' | $3.73{ }^{\circ}$ | $186^{\circ}$ | 0.30' | 554.67' | 7.46' (89.52') | $186.20^{\circ}$ | -. $30{ }^{\prime}$ | -0.05' | -7.42' | -0.81' |
| 560' | $3.00{ }^{\circ}$ | $177^{\circ}$ | 0.29' | 559.66' | 7.76' (93.12') | $186.10^{\circ}$ | -.29' | -0.01' | -7.71' | -0.82' |
| 565' | $2.74{ }^{\circ}$ | $187^{\circ}$ | 0.25' | 564.65' | 8.00' (96.00') | $185.90^{\circ}$ | -.25' | -0.01' | -7.96' | -0.83' |
| 570' | $2.93{ }^{\circ}$ | $191^{\circ}$ | 0.25' | 569.64' | 8.25' (99.00') | $186.00^{\circ}$ | -.24' | -0.04' | -8.21' | -0.87' |
| 575' | $2.93{ }^{\circ}$ | $191^{\circ}$ | 0.26' | 574.63' | 8.51' (102.12") | $186.20^{\circ}$ | -.25' | -0.05' | -8.46' | -0.91' |
| 580' | $2.41{ }^{\circ}$ | $184^{\circ}$ | 0.23' | 579.62' | 8.74' (104.88") | $186.20^{\circ}$ | -.23' | -0.03' | -8.69' | -0.95' |
| 585' | $2.57^{\circ}$ | $196{ }^{\circ}$ | 0.22' | 584.61' | 8.95' (107.40') | $186.30^{\circ}$ | -.21' | -0.04' | -8.90' | -0.98' |
| 590 | $2.31^{\circ}$ | $183^{\circ}$ | 0.21' | 589.60' | 9.16' (109.92') | $186.40^{\circ}$ | -.21' | -0.04' | -9.11' | -1.02' |
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## Drift-Pac 3-D Projection View - B-901

## Drift Distance $=$ 9.16 Feet Drift Bearing $=186.4$ Degrees True Vertical Depth $=589.60$ Feet



Depth (Feet)

## Drift-Pac Polar View - B-901 <br> UNAVCO

Drift Distance $=$ 9.16 Feet $\quad$ Drift Bearing $=186.4$ Degrees $\quad$ True Vertical Depth $=589.60$ Feet


## DRIFT-PAC METHODOLOGY

## Balanced Tangential Method

The Balanced Tangential Method uses the inclination and direction angles at the upper and lower ends of the course length in a manner so as to balance the two sets of measured angles over a course length. From a theoretical standpoint, this method combines the trigonometric functions to provide the average balanced inclination and direction angles, which are used in standard computational procedures. Other common names for this method are Vector Averaging, Acceleration, and Trapezoidal.


